

## Report initial type test (ITT) "treatment efficiency" of the small wastewater treatment systems for up to 50 PT conform EN 12566-3:2005

Range "BioKube Aerated Wastewater Treatment System"

**Of BioKube** 

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Translated version

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Annex 2 : Scaling rules used by the manufacturer

## 1 Introduction

This document is the report covering the initial type tests in compliance with EN12566-3+A1 of the range small wastewater treatment systems of Biokube.

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## 2 **Procedure Initial Type Tests (ITT)**

The initial type tests (ITT) were conducted in compliance with:

*EN* 12566-3: Small wastewater treatment systems for up to 50 PT - part 3: Packaged and/or site assembled domestic wastewater treatment plants

European Construction Products Directive EG/89/106

More specifically it concerns:

• <u>ITT treatment efficiency</u> EN 12566-3, Annexe B

## **3 Product specifications**

The BioKube range of AWTS (Aerated Wastewater Treatment System) is based on the technology of biological degrading of organic material via natural bacteria living on submerged aerated filters (SAF or submerged aerated filter).

The phosphorus removal kit was not in operation during the testing.

#### <u>Durbility</u>

The BioKube range of AWTS mentioned in this report uses PP as base-material. According to the manufacturer, the properties are already known and the used materials comply with EN12566-3, section 6.5.7



#### Technical drawing 1 : BioKube Venus 1850 (5 PE) Venus : internals

- 1. A separate pre-settlement-tank (septic tank /pre cleaning unit) is used (Sebico FAN 3000 liters) (not on the technical drawing)
- 2. The pre-cleaned wastewater is buffered at the bottom of the Venus 1850system and pumped into the first cleaning camber at timed intervals.
- 3. The wastewater flows through the fist SAF (=Submerged Aerated Filter) (BioBlock) and
- 4. is led into a clarification chamber.
- 5. the water gravitates into the second SAF and
- 6. is led into the second clarification camber.

Finally, the cleaned wastewater is discharged .



Technical drawing 2 : BioKube 1850 (5 PE) Venus : Top view

Sludge which settles in each cleaning section, is pumped back to the pre-settlement tank/septic tank several times a day by an airlift. From the pre-settlement tank the sludge should be removed periodically.

#### <u>Control box</u>

The air blowers and technical box is located in the a separate chamber above the volume-buffer (2).

Air blower 1 (cleaning chamber 1 (4) : Model : BA40A Elec : 230 VAC/50Hz ; 0,3A Pressure : 0,13 kg/cm<sup>2</sup> Air volume : 42 L/min

Air blower 2 (cleaning chamber 2 (6) : Model : BA30A Elec : 230 VAC/50Hz ; 0,13 A Pressure : 0,13 kg/cm<sup>2</sup> Air volume : 28 L/min

#### Timers :

Influent pump (2) pause : 15 min; run : 10 sec

Air blower 1 (4): continuous

Air blower 2 (6) : continuous

Airlift 1 (5) : pause : 15 min; run : 10 sec

Airlift 2 (7) : pause : 12 hours; run : 100 sec

Water pump : Pedrollo Vortes 375 W, 220 V

Magnet valve : Mivalt

Biofilter : Exponet 2 pcs Bioblok 100 2 pc bioblok 200

Diffuser : 2 pcs Gummijager GD 270

## 4 ITT Treatment efficiency

#### 4.1 Test rig

The BioKube Venus 1850 (5 PE) Venus was set up in the Certipro<sup>®</sup> test facility on November 22 2007, in accordance with the installation instructions for the system (see photo 1). The Micro station was hydraulically loaded to 5 PE in accordance with EN 12566-3. This report includes the results of this test.



Photo 1: left : BioKube Venus 1850 (5 PE) set up in Certipro<sup>®</sup> test facility right : pre-settlement tank (septic tank) left : BioKube Venus 1850 (5 PE)

#### **Dimensional inspection**

#### Tank 1 (FAN 3000 liters Sebico)

Dimension (cm)	Technical drawing	Value measured
Height	147	147
Length	255	255
Width	123	123
Dia In/out	10	10
Height out	127	127

Table 1: BioKube 5 FAN 3000 Sebico : dimensions

#### Tank 2 (BioKube Venus 1850 5( PE)):

Dimension (cm)	Technical drawing	Value measured
Diameter tank	110	110
Height tank (without cover)	183	183
Min. height volume buffer	25	183-157=26
In/Out/sludge return	11	11

Table 2: BioKube Venus 1850 (5 PE) dimensions

#### 4.2 Test schedule

The initial 38-week type test was started up following a stabilization period of 1 month.

Sequence	Characteristic	Start	End
1	Biomass establishment	22/11/07	30/12/07
2	Nominal	30/12/07	13/02/08
3	Under loading 50 %	13/02/08	27/02/08
4	Nominal PBD	27/02/08	09/04/08
5	Low occupation stress 0%	09/04/08	23/04/08
6	Nominal	23/04/08	09/05/08
extra	Recovery	19/05/08	02/06/08
6	Nominal	02/06/08	25/06/08
7	Overloading 150%	25/06/08	09/07/08
8	Nominal PBD	09/07/08	20/08/08
9	Under loading 50%	20/08/08	03/09/08
10	Nominal PBD	03/09/08	18/10/08
7	Overloading	18/10/08	29/10/08
extra	150%		

Table 3: Test schedule for the BioKube Venus 1850 (5 PE)

Abnormalities and deviations during test procedure

Sequence 1 : one sample hasn't been taken due to malfunction of the automated sampling machine. Extra sample was taken during sequence 10

19/05/08: observation : electrical power supply has been interrupted. The cause of this power cut was not within the BioKube system.

The system was given 14 days for biomass re-establishment after the power was reconnected at 19/05/08. The log-data shows the fault occurred from O9/05/08

01/07/08: Sludge-return-valve was found to be defective and was replaced. It is not known when the malfunction occurred, last samples (as from 11/06/08) were rejected since these samples might be compromised due to the malfunction. Extra samples were taken during sequence 10.

8/07/08 : influent out of specs : test sequence re-done after sequence 10

#### 4.3 Influent properties

The BioKube Venus 1850 (5 PE) was subjected to a daily hydraulic loading of 750 liters/day, dosed in accordance with the dosing schedule below (table 4). The influent was fed into the system by gravity in 25-litre batches. The dosages were uniformly distributed over a dosing period, the number of which was dependent upon the dosing period. The BioKube Venus 1850 (5 PE) was also subjected to a weekly bathwater test (peak flow discharge). During the peak throughput of 40%, an additional quantity of 2\*200 liters per 3 minutes of waste water was fed through the system.

time	Percentage daily throughput
3h00	30
3h00	15
6h00	0
2h00	40
3h00	15
7h00	0

Table 4: BioKube Venus 1850 (5 PE) dosage schedule

Raw household waste water was used during the test procedure. The influent properties listed below require to be achieved in order to be able to use the corresponding effluent results for evaluation:

BOD<sub>5</sub>: 150 - 500 mg/l or COD: 300 - 1000 mg/l Suspended solids: 200 - 700 mg/l Kjel N: 25 - 100 mg/l of NH<sub>4</sub>-N: 22 - 80 mg/l P<sub>T</sub>: 5 - 20 mg/l

#### 4.4 Test results

Analy	vsis results	from the	24-hour	effluent and	d according	g influent	samples	in accordance	e with the to	est schedule ar	e listed below.
							1				

			WK 2	WK 3	WK 7	WK 7	WK 9	WK 10	WK 11	WK 12	WK 13	WK 15
	рН						6,74			0	7,36	7,75
I	Sus. S.	mg/L	168	228	275	275	200	225	195	220	230	220
Ν	Set. S.	mL/L					5	9,5	6,5	6,5	9,5	5,5
F	NH4-N	mg N/L	55,6	65	58	58	71	78	65	77	64	69
L	NO2	mg N/L								<0,1	<0,1	<0,1
U	NO3	mg N/L								<0,5	<0,5	<0,5
E	NOx									<0,5	<0,5	<0,5
Ν	Pt	mg P/L	9,91		10,3	10,3	9,68	11,1	10,4	0	11	10,4
Т	Kj-N	mg N/L	82,2	100	78	78	75	90	81	0	87	86
	BOD	mg O2/L	257	257	340	340	270	320	315	275	370	370
	COD	mg O2/L	525	579	805	805	690	745	705	*	680	650
				Sequence 2		Seque	ence 3			Sequence 4	ļ	
			1	nominal load		underl	oading		Noi	minal load F	PBD	
			י 10/01/08	nominal load 17/01/08	12/02/08	underl 17/02/08	oading 26/02/08	4/03/08	Noi 11/03/08	minal load F 18/03/08	25/03/08	8/04/08
F	рН		10/01/08 7,8	nominal load 17/01/08 7,72	12/02/08 7,46	underl 17/02/08 7,72	oading 26/02/08 7,8	4/03/08 7,95	Noi 11/03/08 7,83	minal load F 18/03/08 7,88	PBD 25/03/08 7,79	8/04/08 7,69
E	pH Sus. S.	mg/L	10/01/08 7,8 <4,3	nominal load 17/01/08 7,72 18.71	12/02/08 7,46 10	underl 17/02/08 7,72 5	oading 26/02/08 7,8 6	4/03/08 7,95 4	Noi 11/03/08 7,83 6	minal load F 18/03/08 7,88 28	PBD 25/03/08 7,79 7	8/04/08 7,69 3
E F	pH Sus. S. Set. S.	mg/L mL/L	10/01/08 7,8 <4,3 <0,1	nominal load 17/01/08 7,72 18.71 <5	12/02/08 7,46 10 <0,1	underl 17/02/08 7,72 5 <0,1	oading 26/02/08 7,8 6 <0,1	4/03/08 7,95 4 <0,1	Noi 11/03/08 7,83 6 <0,1	minal load F 18/03/08 7,88 28 <0,1	PBD 25/03/08 7,79 7 <0,1	8/04/08 7,69 3 <0,1
E F F	pH Sus. S. Set. S. NH4-N	mg/L mL/L mg N/L	10/01/08 7,8 <4,3 <0,1 0,808	nominal load 17/01/08 7,72 18.71 <5 1.1	12/02/08 7,46 10 <0,1 5,8	underl 17/02/08 7,72 5 <0,1 1,1	oading 26/02/08 7,8 6 <0,1 <0,1	4/03/08 7,95 4 <0,1 0,2	Noi 11/03/08 7,83 6 <0,1 0,3	minal load F 18/03/08 7,88 28 <0,1 0,1	PBD 25/03/08 7,79 7 <0,1 0,1	8/04/08 7,69 3 <0,1 4
E F L	pH Sus. S. Set. S. NH4-N NO2	mg/L mL/L mg N/L mg N/L	10/01/08 7,8 <4,3 <0,1 0,808 6,21	nominal load 17/01/08 7,72 18.71 <5 1.1 0.21	12/02/08 7,46 10 <0,1 5,8 0,23	underl 17/02/08 7,72 5 <0,1 1,1 0,21	oading 26/02/08 7,8 6 <0,1 <0,1 <0,1	4/03/08 7,95 4 <0,1 0,2 0,1	Noi 11/03/08 7,83 6 <0,1 0,3 <0,1	minal load F 18/03/08 7,88 28 <0,1 0,1 <0,1	PBD 25/03/08 7,79 7 <0,1 0,1 <0,1	8/04/08 7,69 3 <0,1 4 0,43
E F L U	pH Sus. S. Set. S. NH4-N NO2 NO3	mg/L mL/L mg N/L mg N/L mg N/L	10/01/08 7,8 <4,3 <0,1 0,808 6,21 12,5	nominal load 17/01/08 7,72 18.71 <5 1.1 0.21 14	12/02/08 7,46 10 <0,1 5,8 0,23 15	underl 17/02/08 7,72 5 <0,1 1,1 0,21 14	oading 26/02/08 7,8 6 <0,1 <0,1 <0,1 12	4/03/08 7,95 4 <0,1 0,2 0,1 11	Noi 11/03/08 7,83 6 <0,1 0,3 <0,1 12	minal load F 18/03/08 7,88 28 <0,1 0,1 <0,1 11	PBD 25/03/08 7,79 7 <0,1 0,1 <0,1 13	8/04/08 7,69 3 <0,1 4 0,43 17
EFFLUEN	pH Sus. S. Set. S. NH4-N NO2 NO3 NOx	mg/L mL/L mg N/L mg N/L mg N/L	10/01/08 7,8 <4,3 <0,1 0,808 6,21 12,5 18.7	nominal load 17/01/08 7,72 18.71 <5 1.1 0.21 14 14	12/02/08 7,46 10 <0,1 5,8 0,23 15 15	underl 17/02/08 7,72 5 <0,1 1,1 0,21 14 14	oading 26/02/08 7,8 6 <0,1 <0,1 <0,1 12 12	4/03/08 7,95 4 <0,1 0,2 0,1 11 11	Noi 11/03/08 7,83 6 <0,1 0,3 <0,1 12 12	minal load F 18/03/08 7,88 28 <0,1 0,1 <0,1 11 11	PBD 25/03/08 7,79 7 <0,1 0,1 <0,1 13 13	8/04/08 7,69 3 <0,1 4 0,43 17 17,4
EFFLUENT	pH Sus. S. Set. S. NH4-N NO2 NO3 NOx Pt	mg/L mL/L mg N/L mg N/L mg N/L mg P/L	10/01/08 7,8 <4,3 <0,1 0,808 6,21 12,5 18.7 0,398	nominal load 17/01/08 7,72 18.71 <5 1.1 0.21 14 14 8,58	12/02/08 7,46 10 <0,1 5,8 0,23 15 15 8,01	underl 17/02/08 7,72 5 <0,1 1,1 0,21 14 14 8,58	oading 26/02/08 7,8 6 <0,1 <0,1 <0,1 12 12 8,38	4/03/08 7,95 4 <0,1 0,2 0,1 11 11 7,67	Noi 11/03/08 7,83 6 <0,1 0,3 <0,1 12 12 8,15	minal load F 18/03/08 7,88 28 <0,1 0,1 <0,1 11 11 8,7	PBD 25/03/08 7,79 7 <0,1 0,1 <0,1 13 13 8,4	8/04/08 7,69 3 <0,1 4 0,43 17 17,4 8,51
EFFLUENT	pH Sus. S. Set. S. NH4-N NO2 NO3 NOx Pt Kj-N	mg/L mL/L mg N/L mg N/L mg P/L mg N/L	10/01/08 7,8 <4,3 <0,1 0,808 6,21 12,5 18.7 0,398 5,43	nominal load 17/01/08 7,72 18.71 <5 1.1 0.21 14 14 8,58 5.2	12/02/08 7,46 10 <0,1 5,8 0,23 15 15 8,01 10	underl 17/02/08 7,72 5 <0,1 1,1 0,21 14 14 8,58 5,2	oading 26/02/08 7,8 6 <0,1 <0,1 <0,1 12 12 8,38 4,6	4/03/08 7,95 4 <0,1 0,2 0,1 11 11 7,67 3,6	Noi 11/03/08 7,83 6 <0,1 0,3 <0,1 12 12 12 8,15 3,1	minal load F 18/03/08 7,88 28 <0,1 0,1 <0,1 11 11 8,7 4,4	PBD 25/03/08 7,79 7 <0,1 0,1 <0,1 13 13 8,4 4	8/04/08 7,69 3 <0,1 4 0,43 17 17,4 8,51 6,9
EFFLUENT	pH Sus. S. Set. S. NH4-N NO2 NO3 NO3 NOx Pt Kj-N BOD	mg/L mL/L mg N/L mg N/L mg P/L mg N/L mg O2/L	10/01/08 7,8 <4,3 <0,1 0,808 6,21 12,5 18.7 0,398 5,43 16,9	nominal load 17/01/08 7,72 18.71 <5 1.1 0.21 14 14 8,58 5.2 5	12/02/08 7,46 10 <0,1 5,8 0,23 15 15 8,01 10 13	underl 17/02/08 7,72 5 <0,1 1,1 0,21 14 14 8,58 5,2 5	oading 26/02/08 7,8 6 <0,1 <0,1 <0,1 12 12 8,38 4,6 6	4/03/08 7,95 4 <0,1 0,2 0,1 11 11 7,67 3,6 4	Noi 11/03/08 7,83 6 <0,1 0,3 <0,1 12 12 12 8,15 3,1 7	minal load F 18/03/08 7,88 28 <0,1 0,1 0,1 11 11 8,7 4,4 6	PBD 25/03/08 7,79 7 <0,1 0,1 <0,1 13 13 13 8,4 4 6	8/04/08 7,69 3 <0,1 4 0,43 17 17,4 8,51 6,9 5

\* : no value determined

			WK 23	WK 24	WK 29	WK 31	WK 32	WK 33	WK 34
	pН		7,02	7,09	7,13	7,06	7,02	7,83	7,15
1	Sus. S.	mg/L	225	340	290	695	220	225	190
Ν	Set. S.	mL/L	7,5	11	7,5	17	7	11	10
F	NH4-N	mg N/L	68	74	77	48	60	76	71
i	NO2	mg N/L	<0,1	<0,1	<0,1	<0,1	<0,1	<0,1	<0,1
ū	NO3	mg N/L	<0,5	<0,5	<0,5	<0,5	<0,5	<0,5	<0,5
Ē	NOx		<0,5	<0,5	<0,5	<0,5	<0,5	<0,5	<0,5
	Pt	mg P/L	11,6	13,2	11,3	16,5	10,4	13	11,5
	Kj-N	mg N/L	91	98	100	86	79	98	96
I	BOD	mg O2/L	275	285	290	250	305	230	345
	COD	mg O2/L	710	845	900	1280	635	750	705
			Seque	ence 6			Sequence 8	3	
			Nomin	al load			Nominal loa	d	
			3/06/08	10/06/08	15/07/08	29/07/08	5/08/08	12/08/08	19/08/08
	pН		7,22	7,55	7,76	7,52	7,8	7,82	7,66
Е	Sus. S.	mg/L	20	4	25	22	14	7	8
F	Set. S.	mĹ/L	0,6	<0,1	4	0,7	0,1	<0,1	<0,1
i	NILLA NI								
	INH4-IN	mg N/L	2,4	0,2	34	0,1	0,1	<0,1	<0,1
	NO2	mg N/L mg N/L	2,4 1,4	0,2 0,32	34 3,1	0,1 0,24	0,1 0,15	<0,1 <0,1	<0,1 <0,1
U	NO2 NO3	mg N/L mg N/L mg N/L	2,4 1,4 21,9	0,2 0,32 22,4	34 3,1 9,15	0,1 0,24 17	0,1 0,15 16,6	<0,1 <0,1 20,8	<0,1 <0,1 24,5
UEN	NO2 NO3 NOx	mg N/L mg N/L mg N/L	2,4 1,4 21,9 23,3	0,2 0,32 22,4 22,7	34 3,1 9,15 12,3	0,1 0,24 17 17,2	0,1 0,15 16,6 16,8	<0,1 <0,1 20,8 20,9	<0,1 <0,1 24,5 24,6
L U E N	NO2 NO3 NOx Pt	mg N/L mg N/L mg N/L mg P/L	2,4 1,4 21,9 23,3 9,6	0,2 0,32 22,4 22,7 9,27	34 3,1 9,15 12,3 10,7	0,1 0,24 17 17,2 10,6	0,1 0,15 16,6 16,8 8,71	<0,1 <0,1 20,8 20,9 8,79	<0,1 <0,1 24,5 24,6 9,25
L U E N T	NH4-N NO2 NO3 NOx Pt Kj-N	mg N/L mg N/L mg N/L mg P/L mg N/L	2,4 1,4 21,9 23,3 9,6 5,8	0,2 0,32 22,4 22,7 9,27 4	34 3,1 9,15 12,3 10,7 42	0,1 0,24 17 17,2 10,6 4,3	0,1 0,15 16,6 16,8 8,71 3,4	<0,1 <0,1 20,8 20,9 8,79 2,7	<0,1 <0,1 24,5 24,6 9,25 3
L U E N T	NH4-N NO2 NO3 NOx Pt Kj-N BOD	mg N/L mg N/L mg P/L mg N/L mg O2/L	2,4 1,4 21,9 23,3 9,6 5,8 9	0,2 0,32 22,4 22,7 9,27 4 4	34 3,1 9,15 12,3 10,7 42 19	0,1 0,24 17 17,2 10,6 4,3 8	0,1 0,15 16,6 16,8 8,71 3,4 3	<0,1 <0,1 20,8 20,9 8,79 2,7 <3	<0,1 <0,1 24,5 24,6 9,25 3 3 3

			WK 35	WK 36	WK 37	WK 39	WK 40	WK 41	WK 42	WK 43	WK 44
	рН		7,6	7,16	7,12	7,2	7,63	7,46	7,54	7,55	7,67
I	Sus. S.	mg/L	235	370	280	275	195	550	245	390	340
Ν	Set. S.	mL/L	10	10	7,5	10	12	10	12	12	0,1
F	NH4-N	mg N/L	69	92	66	71	73	75	72	71	70
i	NO2	mg N/L	<0,1	<0,1	<0,1	<0,1	<0,1	<0,1	<0,1	<0,1	<0,1
ū	NO3	mg N/L	<0,5	<0,5	<0,5	<0,5	<0,5	<0,5	<0,5	<0,5	<0,5
E	NOx		<0,5	<0,5	<0,5	<0,5	<0,5	<0,5	<0,5	<0,5	<0,5
	Pt	mg P/L	11,6	14,7	11,8	11,7	10,6	16,2	11,5	12,9	11,5
N	Kj-N	mg N/L	96	98	98	90	91	110	94	110	90
I	BOD	mg O2/L	200	270	295	290	255	250	210	265	255
	COD	mg O2/L	585	900	740	705	530	1180	545	980	630
			Seque	nce 9			Sequence	10		Sequen	ce 10
			Underlo	bading		No	ominal load	PBD		Nominal lo	ad PBD
			26/08/08	2/09/08	9/09/08	23/09/08	30/09/08	8/10/08		22/10/08	28/10/08
	рН		7,72	7,37	7,11	7,14	7,5	7,51	7.45	7,54	7,42
Е	Sus. S.	mg/L	10	57	38	7	4	6	6	4	7
F	Set. S.	mL/L	0,1	1,9	0,9	<0,1	<0,1	<0,1	0,1	<0,1	<0,1
L	NH4-N	mg N/L	<0,1	<0,1	<0,1	0,7	0,3	<0,1	0,3	0,4	0,4
ū	NO2	mg N/L	<0,1	<0,1	<0,1	0,52	0,32	<0,1	0,15	0,33	0,39
F	NO3	mg N/L	20,6	24,7	32,9	27.5	27,6	25	22	23	40,00
	NOx		20,6	24,7	33	28	27,9	25	22	24	41
	Pt	mg P/L	11,5	11,1	12,5	10,8	10	10,2	10,4	8,12	10,5
I	Kj-N	mg N/L	3	5,6	5,5	5,8	3,4	2,6	3,6	2,9	3,4
	BOD	mg O2/L	<3	7	10	11	4	3	4	4	4
	COD	ma O2/L	38	98	110	80	71	69	73	65	55

Table 5: BioKube Venus 1850 (5 PE): analytical data

Sus. S :Suspended solids $NOx = NO_2 + NO_3$ Set. S. : settable solids

Kj-N = Kjeldahl nitrogen

Pt : total phosphate

#### 4.4.1 Evaluation of thet results

All chemical analysis were done under BELAC accreditation. BELAC is the Belgian accreditation body and member of EA (European Accreditation).

The treatment performance of the BioKube Venus 1850 (5 PE) Venus micro station was established by means of a sampling test consisting of 20 mixed samples taken (24 h) spread during the sequences with nominal lo ad (5 PT).

 $\label{eq:pH} \begin{array}{l} pH = 7,6\\ SS_{nom\ average} = 11,9\ mg/l\\ \text{Settleable\ solids_{nom\ average}} = 0,4\ ml/l\\ \text{NH4-N}_{nom\ average} = 2,5\ mg/l\ N\\ \text{NO}_{x\ nom\ average} = 19,3\ mg/l\ N\\ P_{nom\ average} = 8,97\ mg/l\ P\\ \text{KJ-N}_{nom\ average} = 6,3\ mg/l\ N\\ \text{BOD}_{nom\ average} = 7,3\ mg/l\ O_2\\ \text{COD}_{nom\ average} = 81\ mg/l\ O_2 \end{array}$ 

The average of removal percentages obtain during the periods with nominal load are:

 $\begin{array}{l} BOD_{red\%} = 97 \ \% \\ COD_{red\%} = 89 \ \% \\ SS_{red\%} = 96 \ \% \\ NH4\text{-}N_{red\%} = 96 \ \% \end{array}$ 

The removal percentages obtained during 50% charge sequences :

Parameter	sample 1	sample 2	sample 3	sample 3
BOD <sub>red%</sub> (mg/l)	99 %	98 %	>99 %	97 %
COD <sub>red%</sub> (mg/l)	92 %	91 %	94 %	89 %
SS <sub>red%</sub> (mg/l)	98 %	97 %	96 %	85 %
Pt red% (mg P/l)	17 %	13 %	1 %	24 %

Table 6 : individual removal percentages 50 %-charge

And 150 %-charge (overloading)

Parameter	sample 1	sample 2
BOD <sub>red%</sub> (mg/l)	98	98
COD <sub>red%</sub> (mg/l)	93	91
SS <sub>red%</sub> (mg/l)	99	98
$P_{t red\%}$ (mg P/l)	37	9

Table 7 : individual removal percentages 150 %-charge

#### 4.4.2 Summary of interventions

As mentioned in chapter 4.2 "Test schedule", there was an electrical power cut as from 09/05/08 up to 19/05/08. This power cut was not due to the BioKube system but was caused by the technical system of Certipro. The system was given 14 days recovery period.

01/07/2008 : BioKube placed a bumper over de outlet. This should prevent the excessive loss of sludge. The defective "sludge-return-valve" was replaced.



**<u>Photo 2</u>** : detail : bumper over the outlet;

#### 4.4.3 Electrical power consumption

The electrical power consumption during the test procedure was 442 kWh (from 23/11/2007 up to 29/10/2008). The average daily consumption was 1,35 kWh and the annual consumption for the Micro station will be approximately 473 kWh.

#### 4.4.4 Sludge production

The BioKube Venus 1850 (5 PE) was started up without inoculation of activated sludge.

The sludge, which settles in each cleaning section, is pumped back to the presettlement tank/septic tank several times a day by an airlift.

Therefore, there was no sludge accumulation in botch cleaning sections. The total sludge mass of the Biofilm and the activated sludge in the reactor chambers is negligible to the sludge accumulation in the pre-settlement tank.

There was no sludge removed from the system during the test;

The final sludge concentrations in the pre-settlement tank was 1,6 g/l (19/11/2008).

The total quantity of sludge produced during 363 days was 4, 8 kg (d.m.) Sludge level pre-settlement tank : 30 cm, 32 cm, 35 cm (19/11/2008)

#### 4.4.5 Fault detection system assessment

A fault detection system is present and concentrates mainly on the power supply to the compressors.

#### 4.4.6 Installation and operating instructions

Installation and operating instructions are present.

#### 4.4.7 General overvieuw of the scaling rules used by the manufacturer

Note : Detailed scaling rules can be found in annex 2

<b>Daily</b>	amount	of	water	in	<b>BioKube</b>	systems	to	achieve	a	given	cleaning
requir	<u>ement</u>										

Outlet requirement / BioKube system	BOD<10 NH4<5 (mg/litre)	BOD<20 NH4<20 (mg/litre)	BOD<25 (mg/litre)	BOD<30 (mg/litre)	BOD<40 (mg/litre)
Pluto	N/A (will not fulfil demand)	N/A (will not fulfil demand)	750 litres. 5 PE	750 litres. 5 PE	1050 litres 7 PE
Venus 1850	750 litre 5 PE	1000 litre 7 PE	1500 litre 10 PE	1500 litre 10 PE	
Venus 2200	1500 litre 10 PE	2250 litre 15 PE	3000 litre 20PE	3000 litre 20 PE	
Mars 3000 2K	3000 litre 20 PE	3750 litre 25 PE	4500 litre 30PE	5250 litre 35PE	
Mars 3000 3K	4500 litre 30 PE	5250 litre 35 PE	6000 litre 40 PE	6750 litre 45 PE	
Mars 3000 4 K	6000 litre 40 PE	6750 litre 45 PE	7500 litre 50 PE	8000 litre 55 PE	

<u>Specification of 1 PE</u> (<u>Personnel Equivalent</u>)

One PE equals: Up to 60 gram BOD/day Up to 200 litre water/day.

In table above the daily water consumption is 150 litre/day pr. PE.

If the amount of water is below or above 150 litre/day pr. PE then this fluctuation in incoming amount of water is handled by BioKubes patent of timed inflow.

## Annex 1

## **Technical drawings**

BioKube Venus 1850 (5 PE)



Annex 2

Scaling rules used by the manufacturer



Treatment efficiency calculations after CEN 12566-3 section 6.3 and section B.5 i) based on CEN 12566-3 test from CERTIPRO

## Manufactures Design calculations in regards to test and approval according to CEN 12566-3 for BioKube wastewater systems 5 – 50 PE



BioKubes design calculations in this document cover size calculations in two respects: BioKube Venus 1850 is measured under CEN 12566-3 test specifications, to have a cleaning capability of BOD = 7.3 mg/l for 750 litre of wastewater pr. day.

- a) It is calculated how much waste water each of the different BioKube systems Mars, Venus and Pluto (all of which are based on the same basic technology) will treat if the cleaning requirements are BOD < 10 mg/l. (Same cleaning requirements as measured Venus 1850, calculation on water amount only)
- b) It is calculated how much water each of the different BioKube systems will treat if the cleaning requirements are BOD < 10 mg/l, BOD < 25 mg/l, BOD < 30 mg>l og BOD < 50 mg/l (larger amounts of water can be treated in a given system if the cleaning requirements are less stringent).</li>

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# Preface

BioKube wastewater treatment systems are designed and certified in accordance with the standards described in CEN 12566-3.

The measurements behind said certification were performed at CertiPro, Certification and Testing department of Vito, Boeretang 200, B-2400 Mol, Belgium.

The testing was preformed during the period 22/11/2007 to 29/10/2008.

The tests showed the following average cleaning results:

BOD <sub>5</sub> :	7.3 mg/l	(reduction 97 %)
COD	81 mg / I	(reduction 89 %)
NH4-N	2.5 mg/l	(reduction 96 %)
SS	11.9 mg/l	(reduction 96 %)

The measurements at CertiPro were preformed on a BioKube Venus 5 PE system. In this document nominated as BioKube 1850 to differentiate it from the different models.

# Size calculations for different system sizes from 5 - 50 PE and with different cleaning demands on the outgoing water.

The test results from CertiPro and BioKubes documented and verified size calculations are used to calculate the amount of water (i.e. also number of PE) different BioKube systems can clean.

The amount of water (number of PE) a given system can clean depends on the outlet requirements in the area where the system is installed. The more stringent the outlet requirements, the smaller amount of water can be treated. And vice versa, the less stringent the outlet requirements, the larger amount of water a system can clean.

The amount of water a system can clean to a given outlet demand also depends on the content of the incoming sewage water to be treated. In this document it is assumed that the incoming sewage water is standard household sewage water as defined in CEN 12566-3 section B.3.2.: BOD<sub>5</sub> 150 mg/l to 500 mg/l, or COD 300 mg/l to 1.000 mg/l SS 200 mg/l to 700 mg/l KN 25 mg/l to 700 mg/l or HN4 – N 22 mg/l to 80 mg/l P<sub>tot</sub> 5 mg/l to 20 mg/l

The systems documented in this paper are: BioKube Venus 1850. (In test at CertiPro nominated BioKube Venus 5 PE) BioKube Venus 2200. BioKube Mars 3000 / 2 chambers. BioKube Mars 3000 / 3 chambers. BioKube Mars 3000 / 4 chambers. BioKube Pluto. For the BioKube systems listed above, there is in this document for each system given figures on how much water each system will clean to the following outlet demands:  $BOD_5 < 10 \text{ mg/l}$  and NH4-N < 5 mg/l and SS < 15 mg/l $BOD_5 < 20 \text{ mg/l}$  and NH4-N < 20 mg/l and SS < 20 mg/l $BOD_5 < 25 \text{ mg/l}$  and SS < 30 mg/l $BOD_5 < 30 \text{ and } SS < 30 \text{ mg/l}$  $BOD_5 < 40 \text{ and } SS < 50 \text{ mg/l}$ Given that incoming sewage water to be treated is standard household sewage water as defined above.

#### **Regarding number of PE**

These are based on incoming BOD of 60 g/day per person and 150 l of water per day. If the amount of water differs per person then the difference in water is regulated via timed inflow into the system being changed at setup of the system. The amount of BOD pr. PE is still assumed to be 60 gram BOD pr person pr. day. This adjustment is part of BioKubes patent.

## **BioKube design calculation basis.**

The size calculations for BioKube systems are based on the following material:

- 1. **Degrading ability pr m<sup>2</sup> of BioBlock filters** Se detailed graph on page 7 - 8.
- 2. BioKube verification of cleaning ability for over 2.200 systems installed in Denmark. BioKube design theory in tables on page 2 – 4 verifies in live field tests on 700 systems installed at individual houses in Denmark the theory behind BioKubes calculations.
- 3. BioKube patent US 7,476,321 B2

This patent covers the basis of how the flow of water through a BioKube system is controlled.

BioKube patent (pending) WO 2009/047230 A1
 This patent covers the basic construction and hydraulic flow of BioKube 5 – 50 PE systems.

## Built in overcapacity for increased stability.

All BioKube systems are put on the market with a built in "over capability" of approx 25 %. This built in over capability means there always will be a very stable performance from a BioKube systems and that a BioKube system does not have any problems with unexpected overload in the incoming water.

## The BioKube systems, general overview of cleaning capability.

Outlet					
requirement	BOD<10	BOD<20	BOD<25	BOD<30	BOD<40
/	NH4<5	NH4<20	(mg/litre)	(mg/litre)	(mg/litre)
BioKube	(mg/litre)	(mg/litre)			
system					
Pluto	N/A	N/A	750 litres.	750 litres.	1050 litres
	(will not fulfil	(will not fulfil	5 PE	5 PE	7 PE
	demand)	demand)	Section 1.3	Section 1.3	Section 1.4
Venus 1850	750 litre	1000 litre	1500 litre	1500 litre	
	5 PE	7 PE	10 PE	10 PE	
	Section 2.1	Section 2.2	Section 2.3	Section 2.3	
Venus 2200	1500 litre	2250 litre	3000 litre	3000 litre	
	10 PE	15 PE	20PE	20 PE	
	Section 3.1	Section 3.2	Section 3.3	Section 3.3	
Mars 3000 2K	3000 litre	3750 litre	4500 litre	5250 litre	
	20 PE	25 PE	30PE	35PE	
	Section 4.1	Section 4.2	Section 4.3	Section 4.4	
Mars 3000 3K	4500 litre	5250 litre	6000 litre	6750 litre	
	30 PE	35 PE	40 PE	45 PE	
	Section 5.1	Section 5.2	Section 5.3	Section 5.4	
Mars 3000 4 K	6000 litre	6750 litre	7500 litre	8000 litre	
	40 PE	45	50	55 PE	
	Section 6.1	Section 6.2	Section 6.3	Section 6.4	

Table for daily amount of water in BioKube systems to achieve a given cleaning requirement

## Specification of 1 PE (Personnel Equivalent)

One PE equals: Up to 60 gram BOD/day Up to 200 litre water/day.

In table above the daily water consumption is 150 litre/day pr. PE. If the amount of water is below or above 150 litre/day pr. PE then this fluctuation in incoming amount of water is handled by BioKubes patent of timed inflow.

## **BioKube design calculation basis**

For BioKube Venus, Mars and Pluto systems.

#### **BASIC FORMULA FOR AERATED SUBMERGED FILTERTECHNOLOGI**



Qi x Ci - Ra x A = Qu x Cu and: Qi = Qu

and:

A = <u>Qi (Ci – Cu)</u> Ra

#### ASSUMPTION, Ideal blended water:

Ideal blended water in each cleaning step with O2 concentration of minimum 6 mg/l. The ideal blending of water in each cleaning chamber is archived by a combination of timed inflow (giving an even distribution over time of the incoming waste water) and the powerful and continues mixing of water in the aerated chambers by the raising air from the diffusers.

## **BOD treatment / BOD Reduction Ratio.**

The BOD treatment / reduction value is very depended of the concentration of BOD in the water.





From table above the following basic reduction of BOD as a reduction pr.  $m^2$  filter area from a given BOD concentration can be used.

	BOD 500-30 mg/litre	BOD 30- 10 mg/litre (in chamber 2 if
	(in chamber 1)	applicable)
Reduction in gram of BOD	15	2
day/m2 filter surface.		

## NH4 Treatment / NH4 reduction ratio.

Assuming temperature > 5 Celsius.



#### Table 2

From table above following numbers are the Biokube main figures in dimensioning systems.

Ra.	NH4: 80- 5 mg/litre
Filter surface performance	2
Gram NH4 a day/m2 filter	
surface.	

#### Suspended solids.

After each aerated biological cleaning step there is a settlement zone.

The maximum allowed up going water velocity is 1 m/hour. This ensures the sludge in the treated waste water will settle in the bottom of the system and will be cleaned out by the airlift pumps.

#### Equalized load to system.

The buffer tank size in the BioKube system is 15-30% of daily load. This assures the capability og efficient timed inflow.

## Pluto system 750 litre a day.

Cleaning level: BOD<25 mg/litre, COD<125 mg/litre, SS <35 mg/litre).



Ingoing water. BOD mg/litre	Outgoing water. BOD mg/litre	BOD load gram/day	BOD reduction, Gram BOD m2/day (table 1). (filter surface performance)	submerged filter surface needed. (m2)
300	30	203	15	14
30	25	3,75	2	2
		Filter Surface mg/litre Filter surface p (BioBlock 100)	needed for BOD reduction to 10 present in Pluto	16 32,0
		Because of t =16 m2 the BOD5 in a Pl	he extra filter surface (32-16) e lower theoretical limit for luto is 5-7 mg/litre.	

## Pluto system 1050 litre a day.

Cleaning level: BOD<40 mg/litre, COD<150 mg/litre, SS <50 mg/litre).



Ingoing water. BOD mg/litre	Outgoing water. BOD mg/litre	BOD load gram/day	BOD reduction, Gram BOD m2/day (table 1). (filter surface performance)	submerged filter surface needed. (m2)
300	40	273	15	18
		Filter Surface mg/litre	needed for BOD reduction to 40	18
		Filter surface p	present in Pluto	
		(BioBlock 100)		32,0
		Because of t =14 m2 the BOD5 in a Pl	he extra filter surface (32-18) e lower theoretical limit for luto is 5-10 mg/litre.	

#### Section 2.1

## Venus 1850 system 750 litre a day.

Cleaning level: BOD<10 mg/litre, COD<75 mg/litre, NH4<5 mg/litre, SS <15 mg/litre).



			BOD reduction, Gram BOD	
Ingoing water.	Outgoing water.	BOD load	m2/day (table 1).	submerged filter surface
BOD mg/litre	BOD mg/litre	gram/day	(filter surface performance)	needed. (m2)
300	30	203	15	14
30	10	15	2	7,5
		Filter Surface	needed for BOD reduction to $10$	
		mg/litre		21,5
		Filter surface p	present in Venus 1850	
		(1. chamber Bi	oblok 100).	32,0
		Because of	the extra filter surface (32-	
		21,5) = 10,	5 m2 the theoretical lower	
		limit for BC	DD5 in a Venus 1850 is 5-7	
		mg/litre.		
			NH4 reduction, gram NH4	
Ingoing water.	Outgoing water.	NH4 load	m2/day (table 1).	submerged filter surface
NH4 mg/litre	NH4 mg/litre	gram/day	(filter surface performance)	needed. (m2)
60	5	41	2	20,5
		Filter Surface	needed for NH4 reduction to 5	
		mg/litre.		20,5
		Filter surface p	present in Venus 1850.	
		(2. chamber –	Bioblock 200).	32
		Because of	the extra surface is (32-20,5)	
		= 9,5 m2, tl	he theoretical lower limit for	
		NH4 in a	Venus 1850 is close to 1-2	
		mg/litre.		

#### Section 2.2

## Venus 1850 system 1000 litre a day.

Cleaning level: BOD<20 mg/litre, COD<100 mg/litre, NH4<10 mg/litre, SS <35 mg/litre).



Ingoing water. BOD mg/litre	Outgoing water. BOD mg/litre	BOD load gram/day	BOD reduction, Gram BOD m2/day (table 1). (filter surface performance)	submerged filter surface needed. (m2)
300	30	270	15	18
30	20	10	2	5
		Filter Surface mg/litre	needed for BOD reduction to 20	23
		Filter surface p (1. chamber B	oresent in Venus 1850 ioblok 100).	32,0
		Because of 23) = 9 m2 t BOD5 in a V	the extra filter surface (32- the theoretical lower limit for enus 1850 is 10-15 mg/litre.	
Ingoing water. NH4 mg/litre	Outgoing water. NH4 mg/litre	NH4 load gram/day	NH4 reduction, gram NH4 m2/day (table 1). (filter surface performance)	submerged filter surface needed. (m2)
60	10	50	2	25
		Filter Surface mg/litre.	needed for NH4 reduction to 10	25
		Filter surface p (2. chamber –	present in Venus 1850. Bioblock 200).	32
		Because of a 7 m2 the th in a Venus 1	the extra surface is (32-25) = eoretical lower limit for NH4 850 is 5-10 mg/litre.	

## Venus 1850 system 1500 litre a day.

Cleaning level: BOD<25 mg/litre, COD<125 mg/litre, NH4<30 mg/litre, SS <35 mg/litre).



			BOD reduction, Gram BOD	
Ingoing water.	Outgoing water.	BOD load	m2/day (table 1).	submerged filter surface
BOD mg/litre	BOD mg/litre	gram/day	(filter surface performance)	needed. (m2)
300	30	405	15	27
30	25	7,5	2	3,8
		Filter Surface	needed for BOD reduction to 30	
		mg/litre		31
		Filter surface p	present in Venus 1850	
		(1. chamber B	ioblok 100).	32,0
		The demana	for BOD5 in a Venus 1850 is	
		already fulfi	lled in the 1 <sup>st</sup> chamber. In the	
		2. chamber	the BOD will be reduced	
		down to 10-	15 mg/litre.	
			NH4 reduction, gram NH4	
Ingoing water.	Outgoing water.	NH4 load	m2/day (table 1).	submerged filter surface
NH4 mg/litre	NH4 mg/litre	gram/day	(filter surface performance)	needed. (m2)
60	30	45	2	22,5
		Filter Surface	needed for NH4 reduction to 30	
		mg/litre.		22,5
		Filter surface p	present in Venus 1850.	
		(2. chamber –	Bioblock 200).	32
		Because of	the extra surface is (32-22,5)	
		= 9,5 m2 th	ne theoretical lower limit for	
		NH4 in a Vei	nus 1850 is 15-20 mg/litre.	

#### Section 3.1

## Venus 2200 system 1500 litre a day.

Cleaning level: BOD<10 mg/litre, COD<75 mg/litre, NH4<5 mg/litre, SS<15 mg/litre).



Ingoing water. BOD mg/litre	Outgoing water. BOD mg/litre	BOD load gram/day	BOD reduction, Gram BOD m2/day (table 1). (filter surface performance)	submerged filter surface needed. (m2)
300	30	405	15	27
30	10	30	2	15
		Filter Surface mg/litre	needed for BOD reduction to 10	42
		Filter surface p (1. chamber Bi	oresent in Venus 2200 oblok 100).	60
		Because of 42) = 18 m. for BOD5 in	the extra filter surface (60- 2 the theoretical lower limit a Venus 2200 is 5-7 mg/litre.	
Ingoing water. NH4 mg/litre	Outgoing water. NH4 mg/litre	NH4 load gram/day	NH4 reduction, gram NH4 m2/day (table 1). (filter surface performance)	submerged filter surface needed. (m2)
60	5	83	2	41
		Filter Surface mg/litre.	needed for NH4 reduction to 5	41
		Filter surface p (2. chamber –	present in Venus 2200. Bioblock 200).	60
		Because of 1 19 m2 the tl in a Venus 2	the extra surface is (60-41) = heoretical lower limit for NH4 200 is 1-2 mg/litre.	

## Venus 2200 system 2250 litre a day.

Cleaning level: BOD<20 mg/litre, COD<100 mg/litre, NH4<10 mg/litre, SS <35 mg/litre).



			BOD reduction, Gram BOD	
Ingoing water.	Outgoing water.	BOD load	m2/day (table 1).	submerged filter surface
BOD mg/litre	BOD mg/litre	gram/day	(filter surface performance)	needed. (m2)
300	30	607	15	41
30	20	22,5	2	11
		Filter Surface	needed for BOD reduction to 20	
		mg/litre		52
		Filter surface p	present in Venus 2200	
		(1. chamber B	ioblok 100).	60
		Because of	the extra filter surface (60-	
		52) = 8 m2	the theoretical lower limit for	
		BOD5 in a V	enus 2200 is 10-15 mg/litre.	
			NH4 reduction, gram NH4	
Ingoing water.	Outgoing water.	NH4 load	m2/day (table 1).	submerged filter surface
NH4 mg/litre	NH4 mg/litre	gram/day	(filter surface performance)	needed. (m2)
60	10	113	2	56
		Filter Surface	needed for NH4 reduction to 10	
		mg/litre.		56
		Filter surface p	present in Venus 2250.	
		(2. chamber –	Bioblock 200).	60
		Because of	the extra surface is $(60-56) =$	
		4 m2 the th	eoretical lower limit for NH4	
		in a Venus 2	250 is 8 - 10 mg/litre.	

#### Section 3.3

## Venus 2200 system 3000 litre a day.

Cleaning level: BOD<25 mg/litre, COD<125 mg/litre, NH4<30 mg/litre, SS<35 mg/litre).



			BOD reduction, Gram BOD	
Ingoing water.	Outgoing water.	BOD load	m2/day (table 1).	submerged filter surface
BOD mg/litre	BODmg/litre	gram/day	(filter surface performance)	needed. (m2)
300	30	810	15	54
30	25	15	2	7,5
		Filter Surface	needed for BOD reduction to 30	
		mg/litre		61,5
		Filter surface p	present in Venus 2200	
		(1. and 2. chan	nber Bioblok 100 and 200).	120
		Because of	the extra filter surface (120-	
		61,5) = 58,	6 m2 the theoretical lower	
		limit for BO	D5 in a Venus 2200 is 15-20	
		mg/litre.		
			NH4 reduction, gram NH4	
Ingoing water.	Outgoing water.	NH4 load	m2/day (table 1).	submerged filter surface
NH4 mg/litre	NH4 mg/litre	gram/day	(filter surface performance)	needed. (m2)
60	30	90	2	45
		Filter Surface	needed for NH4 reduction to 30	
		mg/litre.		45
		Filter surface	present in Venus 2200 for	
		nitrification (2	. chamber – Bioblock 200).	55
		Because of t	he extra surface is (55 - 45) =	
		10 m2 the tl	heoretical lower limit for NH4	
		in a Venus 2	200 is 20-25 mg/litre.	

#### Section 4.1

## Mars 3000 2K system, 3000 litre a day.

Cleaning level: BOD<25 mg/litre, COD<125 mg/litre, SS<35 mg/litre).





Ingoing water. BOD mg/litre	Outgoing water. BODmg/litre	BOD load gram/day	BOD reduction, Gram BOD m2/day (table 1). (filter surface performance)	submerged filter surface needed. (m2)
300	30	810	15	54
30	25	15	2	7,5
		Filter Surface mg/litre	needed for BOD reduction to 25	61,5
		Filter surface p (1. and 2. chan	present in Mars 3000-2K nber Bioblok 100 and 200).	150
		Because of i 61,5) = 88 n for BOD5 i mg/litre.	the extra filter surface (150- n2 the theoretical lower limit in a Mars 3000 2K is 5-7	

#### Section 4.2

## Mars 3000 2K system, 3750 litre a day.

Cleaning level: BOD<25 mg/litre, COD<125 mg/litre, SS<35 mg/litre).





Ingoing water. BOD mg/litre	Outgoing water. BODmg/litre	BOD load gram/day	BOD reduction, Gram BOD m2/day (table 1). (filter surface performance)	submerged filter surface needed. (m2)
300	30	1012	15	67
30	25	18,7	2	9,35
		Filter Surface mg/litre	needed for BOD reduction to 25	76
		Filter surface p (1. and 2. chan	present in Mars 3000-2K nber Bioblok 100 and 200).	150
		Because of i 76) = 73 m. for BOD5 i mg/litre.	the extra filter surface (150- 2 the theoretical lower limit in a Mars 3000 2K is 5-7	

## Mars 3000 2K system, 4500 litre a day.

Cleaning level: BOD<25 mg/litre, COD<125 mg/litre, SS<35 mg/litre).





Ingoing water. BOD mg/litre	Outgoing water. BODmg/litre	BOD load gram/day	BOD reduction, Gram BOD m2/day (table 1). (filter surface performance)	submerged filter surface needed. (m2)
300	30	1215	15	81
30	25	22,5	2	11,25
		Filter Surface mg/litre	needed for BOD reduction to 25	93
		Filter surface p (1. and 2. char	present in Mars 3000-2K nber Bioblok 100 and 200).	150
		Because of 93) = 57 m for BOD5 i mg/litre.	the extra filter surface (150- 2 the theoretical lower limit in a Mars 3000 2K is 5-7	

#### Section 4.4

## Mars 3000 2K system, 5250 litre a day.

Cleaning level: BOD<30 mg/litre, COD<125 mg/litre, SS<35 mg/litre).





Ingoing water. BOD mg/litre	Outgoing water. BODmg/litre	BOD load gram/day	BOD reduction, Gram BOD m2/day (table 1). (filter surface performance)	submerged filter surface needed. (m2)
300	30	1417	15	94
		Filter Surface	needed for BOD reduction to 30 $$	
		mg/litre		94
		Filter surface p	present in Mars 3000-2K	
		(1. and 2. chan	nber Bioblok 100 and 200).	150
		Because of	the extra filter surface (150-	
		94)) = 56 m	2 the theoretical lower limit	
		for BOD5 i	in a Mars 3000 2K is 5-7	
		mg/litre.		

## Mars 3000 3K system, 4500 litre a day.

Cleaning level: BOD<10 mg/litre, NH4<5 mg/litre COD<75 mg/litre, SS<15 mg/litre).





			BOD reduction, Gram BOD	
Ingoing water.	Outgoing water.	BOD load	m2/day (table 1).	submerged filter surface
BOD mg/litre	BODmg/litre	gram/day	(filter surface performance)	needed. (m2)
300	30	1215	15	81
30	10	90	2	45
		Filter Surface	needed for BOD reduction to 30	
		mg/litre		126
		Filter surface p	resent	
		(1. and 2. chan	nber Bioblok 100 and 200).	150
		Because of a	the extra filter surface (150-	
		126) =24 m	2 the theoretical lower limit	
		for BOD5 in	n a Mars 3000 3K is 1 - 2	
		mg/litre.		
			NH4 reduction, gram NH4	
Ingoing water.	Outgoing water.	NH4 load	m2/day (table 1).	submerged filter surface
NH4 mg/litre	NH4 mg/litre	gram/day	(filter surface performance)	needed. (m2)
60	5	247	2	123
		Filter Surface	needed for NH4 reduction to 30	
		mg/litre.		123
		Filter surface	present in Mars 3000 3K for	
		nitrification (3.	chamber – Bioblock 200).	100
		Because of	f the extra surface from	
		chamber 1	and 2 theoretical the lower	
		limit for NH	14 in a Mars 3000 3K is 1-2	
		mg/litre.		

## Mars 3000 3K system, 5250 litre a day.

Cleaning level: BOD<20 mg/litre, NH4<20 mg/litre COD<100 mg/litre, SS<35 mg/litre).





Ingoing water.	Outgoing water.	BOD load	BOD reduction, Gram BOD m2/day (table 1).	submerged filter surface
BOD mg/litre	BODmg/litre	gram/day	(filter surface performance)	needed. (m2)
300	30	1417	15	94
30	20	52	2	26
		Filter Surface	needed for BOD reduction to 30	
		mg/litre		120
		Filter surface p	present	
		(1. and 2. chan	nber Bioblok 100 and 200).	150
		Because of a	the extra filter surface (150-	
		120) = 30 m	12 the theoretical lower limit	
		for BOD5 in	n a Mars 3000 3K is 10-15	
		mg/litre.		
			NH4 reduction, gram NH4	
Ingoing water.	Outgoing water.	NH4 load	m2/day (table 1).	submerged filter surface
NH4 mg/litre	NH4 mg/litre	gram/day	(filter surface performance)	needed. (m2)
60	10	262	2	131
		Filter Surface	needed for NH4 reduction to 30	
		mg/litre.		131
		Filter surface	present in Mars 3000 3K for	
		nitrification (3.	chamber – Bioblock 200).	100
		Because of	f the extra surface from	
		chamber 1 d	and 2 the theoretical limit for	
		NH4 in a Ma	rs 3000 3K is 5-7 mg/litre.	

## Mars 3000 3K system, 6000 litre a day.

Cleaning level: BOD<25 mg/litre, NH4<30 mg/litre COD<125 mg/litre, SS<35 mg/litre).





			BOD reduction, Gram BOD	
Ingoing water.	Outgoing water.	BOD load	m2/day (table 1).	submerged filter surface
BOD mg/litre	BODmg/litre	gram/day	(filter surface performance)	needed. (m2)
300	30	1620	15	108
30	25	30	2	15
		Filter Surface	needed for BOD reduction to 25	
		mg/litre		123
		Filter surface p	present	
		(1. and 2. chan	nber Bioblok 100 and 200).	150
		Because of	the extra filter surface (150-	
		123) = 27 m	n2 the theoretical lower limit	
		for BOD5 in	n a Mars 3000 3K is 15-20	
		mg/litre.		
			NH4 reduction, gram NH4	
Ingoing water.	Outgoing water.	NH4 load	m2/day (table 1).	submerged filter surface
NH4 mg/litre	NH4 mg/litre	gram/day	(filter surface performance)	needed. (m2)
60	30	180	2	90
		Filter Surface	needed for NH4 reduction to 30	
		mg/litre.		90
		Filter surface	present in Mars 3000 3K for	
		nitrification (3	. chamber – Bioblock 200).	100
		Because of t	the extra filter surface 100-90	
		= 10 m2 a	nd the ekstra surface from	
		chamber 1	and 2 the theoretical lower	
		limit for NH	4 in a Mars 3000 3K is 10-20	
		-		

## Mars 3000 3K system, 6750 litre a day.

Cleaning level: BOD<30 mg/litre, NH4<30 mg/litre COD<125 mg/litre, SS<35 mg/litre).





			BOD reduction, Gram BOD	
Ingoing water.	Outgoing water.	BOD load	m2/day (table 1).	submerged filter surface
BOD mg/litre	BODmg/litre	gram/day	(filter surface performance)	needed. (m2)
300	30	1822	15	121
		Filter Surface	needed for BOD reduction to 30	
		mg/litre		121
		Filter surface p	present	
		(1. and 2. chan	nber Bioblok 100 and 200).	150
		Because of	the extra filter surface (150-	
		121) = 29 m	12 the theoretical lower limit	
		for BOD5 ii	n a Mars 3000 3K is 15-20	
		mg/litre.		
			NH4 reduction, gram NH4	
Ingoing water.	Outgoing water.	NH4 load	m2/day (table 1).	submerged filter surface
NH4 mg/litre	NH4 mg/litre	gram/day	(filter surface performance)	needed. (m2)
60	30	200	2	100
		Filter Surface	needed for NH4 reduction to 30	
		mg/litre.		100
		Filter surface	present in Mars 3000 3K for	
		nitrification (3	. chamber – Bioblock 200).	100
		Because of	the extra filter surface in	
		chamber 1	and 2, 29 m2, the theoretical	
		limit for Ma	rs 3000 3K is 10-20 mg/litre.	

## Mars 3000 4K system, 6000 litre a day.

Cleaning level: BOD<10 mg/litre, NH4<5 mg/litre COD<75 mg/litre, SS<15 mg/litre).





			BOD reduction, Gram BOD	
Ingoing water.	Outgoing water.	BOD load	m2/day (table 1).	submerged filter surface
BOD mg/litre	BODmg/litre	gram/day	(filter surface performance)	needed. (m2)
300	30	1620	15	108
30	10	120	2	60
		Filter Surface	needed for BOD reduction to $30$	
		mg/litre		168
		Filter surface p	present	
		(1. and 2. chan	nber Bioblok 100 and 200).	150
		Because of	the extra filter surface from	
		chamber 3	and 4 the 35 m2 the	
		theoretical I	imit for BOD5 in a Mars 3000	
		3K is 5-7 mg	/litre.	
			NH4 reduction, gram NH4	
Ingoing water.	Outgoing water.	NH4 load	m2/day (table 1).	submerged filter surface
NH4 mg/litre	NH4 mg/litre	gram/day	(filter surface performance)	needed. (m2)
60	5	330	2	165
		Filter Surface	needed for NH4 reduction to 30	
		mg/litre.		165
		Filter surface	present in Mars 3000 4K for	
		nitrification (3.	. chamber – Bioblock 200).	200
		Because of	the extra filter surface 200-	
		165 = 35 m	2, the theoretical lower limit	
		for NH4 in	a Mars 3000 4K is 1-2	
		mg/litre.		

## Mars 3000 4K system, 6750 litre a day.

Cleaning level: BOD<20 mg/litre, NH4<20 mg/litre COD<100 mg/litre, SS<35 mg/litre).





Ingoing water.	Outgoing water.	BOD load	BOD reduction, Gram BOD m2/day (table 1).	submerged filter surface
BOD mg/litre	BODmg/litre	gram/day	(filter surface performance)	needed. (m2)
300	30	1822	17	107
30	20	67	2	34
		Filter Surface	needed for BOD reduction to $30$	
		mg/litre		141
		Filter surface p	present	
		(chamber 1. 2. Bioblok 100 and 200).		150
			NH4 reduction, gram NH4	
Ingoing water.	Outgoing water.	NH4 load	m2/day (table 1).	submerged filter surface
NH4 mg/litre	NH4 mg/litre	gram/day	(filter surface performance)	needed. (m2)
60	20	270	2	135
		Filter Surface needed for NH4 reduction to 30		
		mg/litre.		135
		Filter surface	present in Mars 3000 4K for	
		nitrification (	3. chamber and 4. chamber all	
		Bioblock 200).		200
		Because of	the extra filter surface 200-	
		135 = 65 m	2 the theoretical lower limit	
		for NH4 in	a Mars 3000 4K is 10-15	
		mg/litre.		

## Mars 3000 4K system, 7500 litre a day.

Cleaning level: BOD<25 mg/litre, NH4<30 mg/litre COD<125 mg/litre, SS<35 mg/litre).





Ingoing water. BOD mg/litre	Outgoing water. BOD mg/litre	BOD load Gram / day	BOD reduction, Gram BOD m2/day (table 1). (filter surface performance)	submerged filter surface needed. (m2)
300	30	2025	17	119
30	25	37	2	19
		Filter Surface 25mg/litre	e needed for BOD reduction to	148
		Filter surface present (chamber 1. and 2, Bioblok 100 and 200).		150
Ingoing water. NH4 mg/litre	Outgoing water. NH4 mg/litre	NH4 load gram/day	NH4 reduction, gram NH4 m2/day (table 1). (filter surface performance)	submerged filter surface needed. (m2)
60	30	225	2	130
		Filter Surface needed for NH4 reduction to 30 mg/litre.		130
		Filter surface present in Mars 3000 4K for nitrification		200
		Because of the extra filter surface 200- 130 = 70 m2, the theoretical lower limit for NH4 in a Mars 3000 4K is 20-25 mg/litre.		

## Mars 3000 4K system, 8000 litre a day.

Cleaning level: BOD<25 mg/litre, NH4<30 mg/litre COD<125 mg/litre, SS<35 mg/litre).





Ingoing water. BOD mg/litre	Outgoing water. BODmg/litre	BOD load gram/day	BOD reduction, Gram BOD m2/day (table 1). (filter surface performance)	submerged filter surface needed. (m2)
300	30	2160	17	127
30	25	40	2	20
		Filter Surface 25mg/litre	needed for BOD reduction to	148
		Filter surface present (chamber 1. and 2, Bioblok 100 and 200).		150
Ingoing water. NH4 mg/litre	Outgoing water. NH4 mg/litre	NH4 load gram/day	NH4 reduction, gram NH4 m2/day (table 1). (filter surface performance)	submerged filter surface needed. (m2)
60	30	240	2	120
		Filter Surface needed for NH4 reduction to 30 mg/litre.		120
		Filter surface present in Mars 3000 4K for nitrification		
		Because of	the extra filter surface 200-	
		120 = 80 m	2, the theoretical lower limit	
		for NH4 in	a Mars 3000 4K is 20-25	
		mg/litre.		